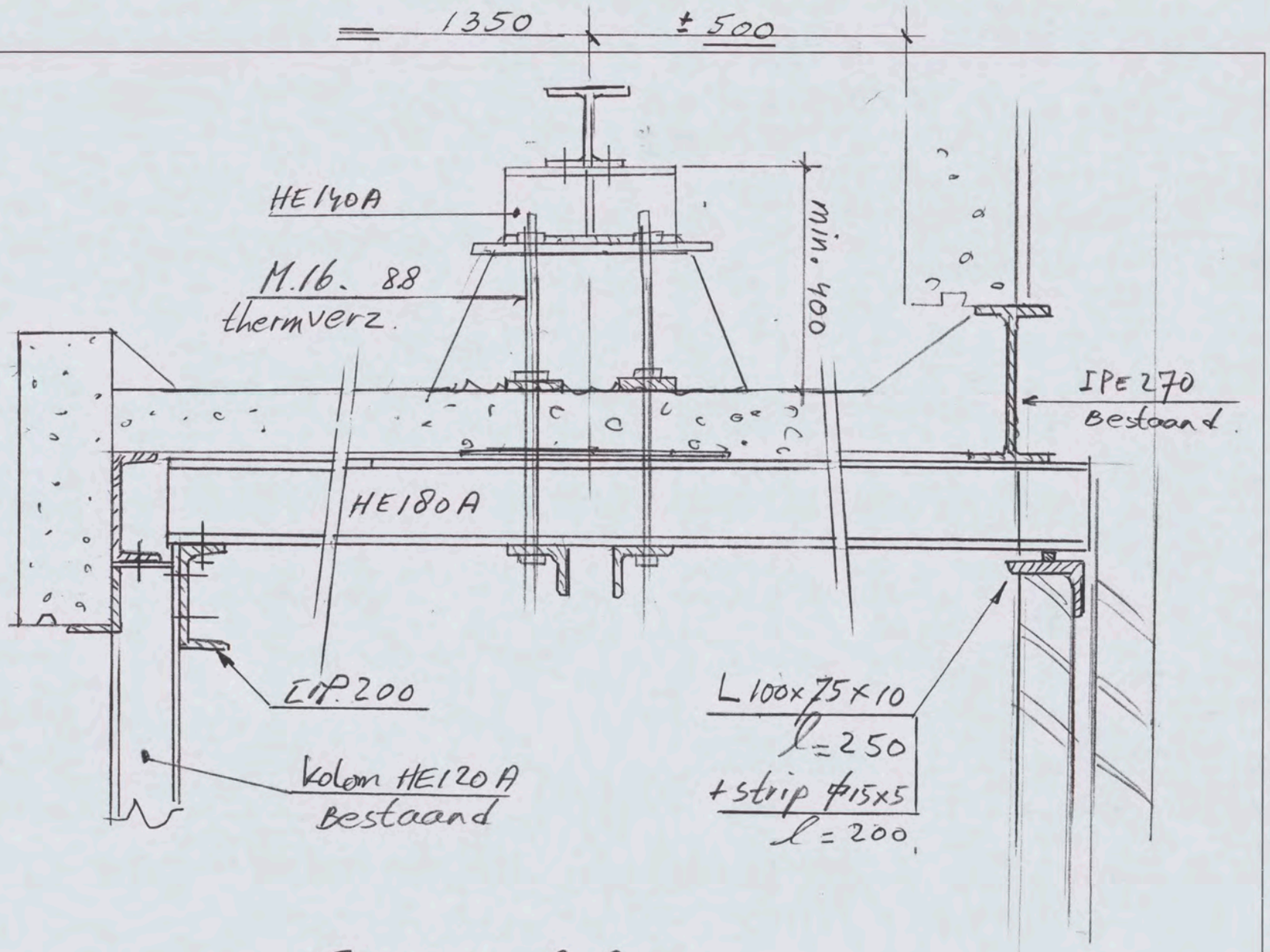


Doorsn. A-A

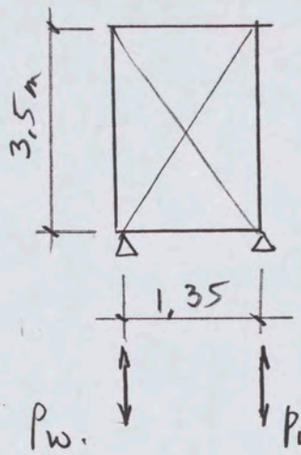
Vervolgblad: 5.3

91.156

Wind op L.6.k.

kastlengte ± 3 m

per zijde

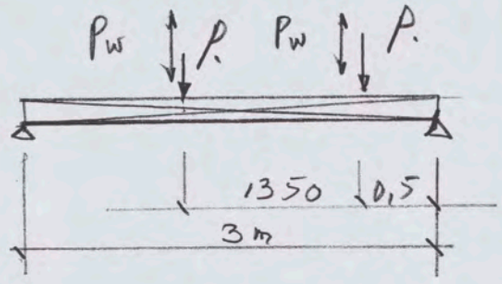


$Q_w = 3{,}5 \times \frac{3}{2} \times 1{,}2 \times 0{,}70 = 5$ kN.

$M = 5 \times \frac{2}{2} = 10$ kN. m.

P_w = trek/druk per $= \frac{10}{1{,}35} = 7{,}5$ kN. rep.

Onderslagbalk v. LBk. +4.000



$P_{vert\ poer\ (e.g)} = 8{,}0$ kN
$P_{wind} = 7{,}5$ kN

$q_{e.g.} = 0{,}75 \times 2{,}5 = 1{,}875$ kN/m'

$q_{nb} = 0{,}75 \times 1{,}5 = 1{,}125$ kN/m'

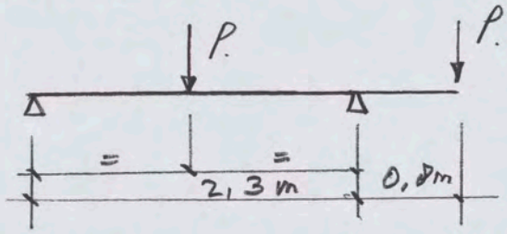
neem HE 180 A

zie comp. ber. bijlage III

$\mu_c = 0{,}308$

max doorbuiging $d = 2{,}8$ mm

Opvangbalk onderslagbalk bij Gevelrand



neem $P_{max.} = 9{,}5$ kN.
$P_{wind} = 3{,}5$ kN.

neem min [NP. 200

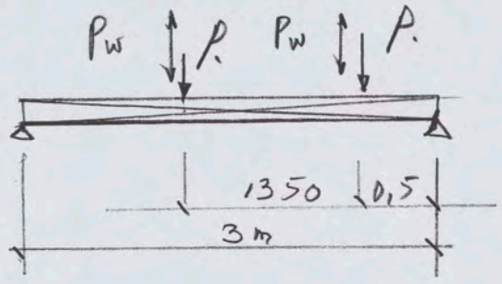
zie comp. ber. bijlage IV

doorbuiging overstek 0,9 mm (permanent.

$\mu_c = 0{,}32$ excl. kip.

neem praktisch [NP. 200

Onderslagbalk v. LBk. +4.000



$P_{vert\ poer\ (e.g)} = 8{,}0$ kN
$P_{wind} = 7{,}5$ kN

$q_{e.g.} = 0{,}75 \times 2{,}5 = 1{,}875$ kN/m'

$q_{nb} = 0{,}75 \times 1{,}5 = 1{,}125$ kN/m'

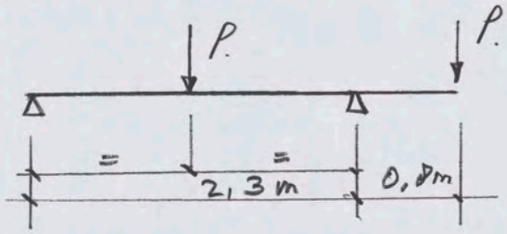
neem HE 180 A

zie comp. ber. bijlage III

$\mu_c = 0{,}308$

max doorbuiging $a = 28$ mm

Opvangbalk onderslagbalk bij Gevelrand



neem $P_{max.} = 9{,}5$ kN.
$P_{wind} = 3{,}5$ kN.

neem min [NP. 200

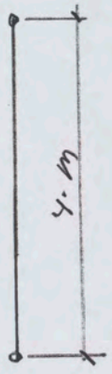
zie comp. ber. bijlage IV

doorbuiging overstek 0,9 mm (permanent.

$\mu_c = 0{,}32$ excl. kip.

neem praktisch [NP. 200

kolom controle HE 120 A (bestaand)



$P_{e.g.} = \left(\frac{3}{2} \times \frac{2,3+6}{2}\right) \times 2,5 = 15,5$ kN

$P_{dakrand} = \frac{2,3+6}{2} \times 2,5 = 10,5$ kN

$P_{Nb.} = \left(\frac{3}{2} \times \frac{2,3+6}{2}\right) \times 1,5 = 9,5$ kN

$P_{koelmach.} =$ 20 kN

$\lambda_z = \frac{4000}{30,2} = 132,5 \therefore \omega = 3,39$

$\sigma_{;d} = 1,5 \frac{55 \times 3,39 \times 10^3}{25,3 \times 10^2} = 110,5$ N/mm^2

$\mu_c = \frac{110,5}{235} = 0,47$ accoord.

Vervolgblad: 6.0

shell Intern. chem. bv. Amsterdam

Fundatie beschouwing geb. 11C
nieuwe situatie

zie ook contr. ber Jacobs proj. NR. 298320
Doc. NR. 303xx/02/1000 7-5-2002

Hierin worden van gebouw 11C de nieuwe kolom/fundatie krachten beschouwd (alleen van de gebouw kolommen)
De krachten geven in deze contr. ber. van Jacobs geen problemen.

zie ook ber. proceffabriek DHV geb. 611
Doss NR. 1-2691-00-10 12-1977

geb. 11 C

beton vloer ± 400 mm dik ↘ 200 mm vulbeton
↘ ± 200 mm. constr. beton.

vloer op palen

N.b. b.gr. vloer = 2000 kg/m² = 20 kN/m² rep.

max. bel. frame kolommen (rekken)

e.g. bordes = 1 kN/m². eg. frame = 1 kN/m².

N.b. bordes = 2,5 kN/m². N.b. frame = 12 kN.m². (alleen op ± 2400)

max. dragend opp. bordes = $1 \times \frac{2,4}{2} \times \frac{1,25}{2} = 0,75 m^2$

max. dragend opp. frame = $1 \times \frac{1,2}{2} \times \frac{1,25}{2} = 0,375$ kN.

kolom belastingen

e.g. = $2 \times (0,75) \times 1 + 2 \times (0,375) \times 1 + (\text{e.g kolom}) \pm 1,25 = 3,5$ kN.

N.b. = $2 \times (0,75) \times 2,5 + 0,375 \times 12 + 0,375 \times 2,5 = 9,2$ kN.

totale kolom bel. = 12,7 kN. rep

pons geen probleem

b.gr. vloer accoord voor frame's (rekken)

hoh. kolommen ± ⌀ 1,25 m en ⌀ 1,5 m.

DHV

Vervolgblad: 6.2.

Overzicht kolomreacties van de onderste kolommen van de staalconstructie (belasting coëff. = 1,5) DHV. 1977

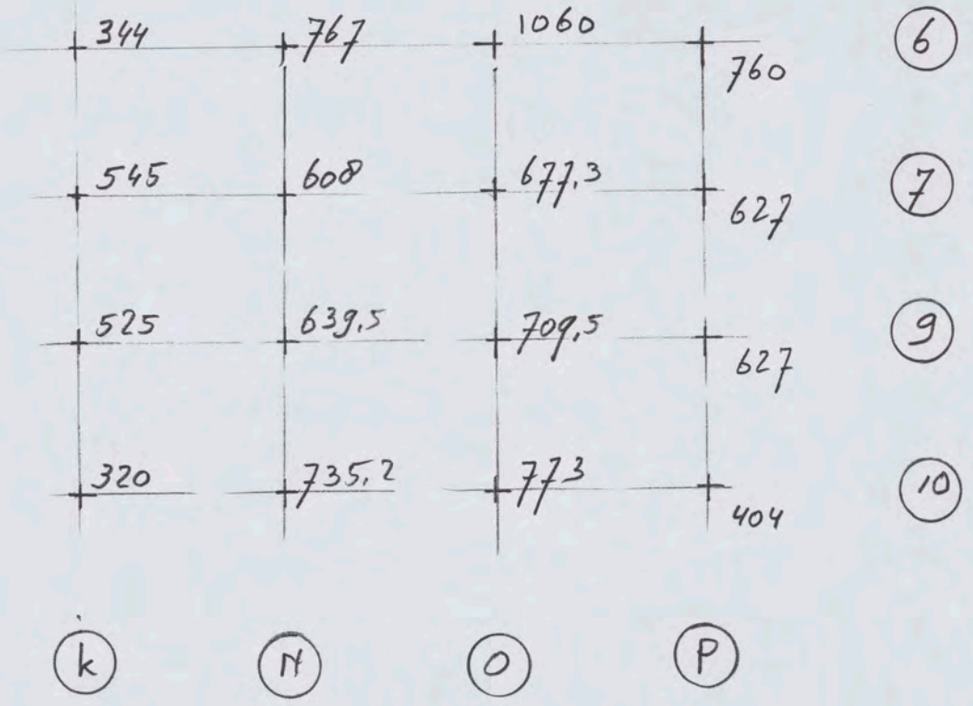
+ 679 (417)	+ 831,1	1071,1	+ 680	(6)
+ 1168,5 (728,6)	+ 852,9	+ 852,9	+ 648,7	(7)
+ 1093,3 (650,4)	+ 852,9	+ 852,9	+ 648,7	(9)
+ 944,9 (644,9)	+ 831,1	+ 831,1	+ 396,6	(10)
(K)	(N)	(O)	(P)	

Huidige situatie

uit DHV. ber. Doss.nr. 1-2691-00-10 12-1977

Overzicht kolomreacties van de onderste kolommen van de staalconstructie

belasting coëff = 1,5



Nieuwe situatie

uit Jacobs berekening doc. 303xx/02/1000

waarin de reductie van e.g. dak van 5 kN/m² naar 2,5 kN/m² is verwerkt

Hiële belasting kolom P.6

$\frac{760}{1,5} \times 1,35 = 684$ kN

accoord.

Vervolgblad:

shell. intern. chem. b.v. Amsterdam

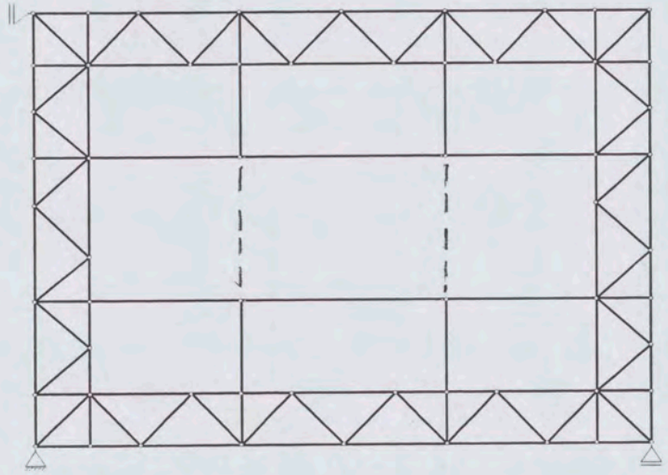
bijlagen

I	stab. krans	bl. 111 t/m 157
II	windligger	bl. 157 t/m 171
III	onderslagbalk L6k. +4.000	bl. 193 t/m 196
IV	dakrandbalk +4.000	bl. 197 t/m. 201

Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250
Dimensies: kN;m;rad (tenzij anders aangegeven)
Datum....: 28/11/2002
Bestand..: c:\documents and settings\ai32075\desktop\technosoft\shell a,dam grid +7.25 ha

Toegepaste norm..: TGB 1990
Theorie voor de bepaling van de krachtsverdeling:
Geometrisch lineair.
Fysisch lineair.

GEOMETRIE



MATERIALEN

Mt	Omschrijving	E-modulus[N/mm2]	S.M.	Pois.	Uitz. coëff	Kruipfactor
1	S235	210000	78.5	0.30	1.2000e-005	

PROFIELEN [mm]

Prof.	Omschrijving	Materiaal	Oppervlak	Traagheid	Vormf.
1	IPE200	1:S235	2.8480e+003	1.9430e+007	0.00
2	UNP200	1:S235	3.2200e+003	1.9110e+007	0.00
3	HEA220	1:S235	6.4300e+003	5.4100e+007	0.00
4	H70/70/11	1:S235	1.4280e+003	6.1800e+005	0.00
5	H70/70/9	1:S235	1.1880e+003	5.2500e+005	0.00
6	H70/70/6	1:S235	1.1880e+003	5.2500e+005	0.00

PROFIELEN vervolg [mm]

Prof.	Staaftype	Breedte	Hoogte	e	Type	b1	h1	b2	h2
1	0:Normaal	100	200	100.0					
2	0:Normaal	75	200	100.0					
3	0:Normaal	220	210	105.0					
4	0:Normaal	70	70	21.3					
5	0:Normaal	70	70	20.5					
6	0:Normaal	70	70	20.5					

the scale towards document
Image Engineering Scan Reference Chart TE263 Serial No. 546
Patch Reference numbers on LITT

Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

KNOPEN

Knoop	X	Z	Knoop	X	Z
1	0.000	0.000	6	12.000	12.600
2	0.000	4.200	7	18.000	12.600
3	0.000	8.400	8	18.000	8.400
4	0.000	12.600	9	18.000	4.200
5	6.000	12.600	10	18.000	0.000
11	12.000	0.000	16	12.000	4.200
12	6.000	0.000	17	0.000	1.500
13	6.000	4.200	18	0.000	7.000
14	6.000	8.400	19	0.000	9.750
15	12.000	8.400	20	0.000	11.100
21	1.600	12.600	26	18.000	11.100
22	3.067	12.600	27	18.000	9.750
23	9.000	12.600	28	18.000	5.600
24	14.932	12.600	29	18.000	2.850
25	16.400	12.600	30	18.000	1.500
31	16.400	0.000	36	1.600	1.500
32	14.933	0.000	37	1.600	2.850
33	9.000	0.000	38	1.600	4.200
34	3.067	0.000	39	1.600	5.500
35	1.600	0.000	40	1.600	8.400
41	1.600	11.100	46	12.000	11.100
42	4.554	11.100	47	13.466	11.100
43	6.000	11.100	48	16.400	11.100
44	7.500	11.100	49	16.400	8.400
45	10.500	11.100	50	16.400	7.000
51	16.400	4.200	56	7.467	1.500
52	16.400	1.500	57	6.000	1.500
53	13.467	1.500	58	4.533	1.500
54	12.000	1.500			
55	10.500	1.500			

STAVEN

St.	ki	kj	Profiel	Aansl.i	Aansl.j	Lengte
1	1	17	1:IPE200	NDM	NDM	1.500
2	17	2	1:IPE200	NDM	NDM	2.700
3	2	18	1:IPE200	NDM	NDM	2.800
4	18	3	1:IPE200	NDM	NDM	1.400
5	3	19	1:IPE200	NDM	NDM	1.350
6	19	20	1:IPE200	NDM	NDM	1.350
7	20	4	1:IPE200	NDM	NDM	1.500
8	4	21	2:UNP200	NDM	NDM	1.600
9	21	22	2:UNP200	NDM	NDM	1.467
10	22	5	2:UNP200	NDM	NDM	2.933
11	5	23	2:UNP200	NDM	NDM	3.000
12	23	6	2:UNP200	NDM	NDM	3.000



Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

STAVEN

St.	ki	kj	Profiel	Aansl.i	Aansl.j	Lengte
13	6	24	2:UNP200	NDM	NDM	2.932
14	24	25	2:UNP200	NDM	NDM	1.468
15	25	7	2:UNP200	NDM	NDM	1.600
16	7	26	1:IPE200	NDM	NDM	1.500
17	26	27	1:IPE200	NDM	NDM	1.350
18	27	8	1:IPE200	NDM	NDM	1.350
19	8	28	1:IPE200	NDM	NDM	2.800
20	28	9	1:IPE200	NDM	NDM	1.400
21	9	29	1:IPE200	NDM	NDM	1.350
22	29	30	1:IPE200	NDM	NDM	1.350
23	30	10	1:IPE200	NDM	NDM	1.500
24	10	31	2:UNP200	NDM	NDM	1.600
25	31	32	2:UNP200	NDM	NDM	1.467
26	32	11	2:UNP200	NDM	NDM	2.933
27	11	33	2:UNP200	NDM	NDM	3.000
28	33	12	2:UNP200	NDM	NDM	3.000
29	12	34	2:UNP200	NDM	NDM	2.933
30	34	35	2:UNP200	NDM	NDM	1.467
31	35	1	2:UNP200	NDM	NDM	1.600
32	36	37	2:UNP200	NDM	NDM	1.350
33	37	38	2:UNP200	NDM	NDM	1.350
34	38	39	2:UNP200	NDM	NDM	1.300
35	39	40	2:UNP200	NDM	NDM	2.900
36	40	41	2:UNP200	NDM	NDM	2.700
37	41	42	2:UNP200	NDM	NDM	2.954
38	42	43	2:UNP200	NDM	NDM	1.446
39	43	44	2:UNP200	NDM	NDM	1.500
40	44	45	2:UNP200	NDM	NDM	3.000
41	45	46	2:UNP200	NDM	NDM	1.500
42	46	47	2:UNP200	NDM	NDM	1.466
43	47	48	2:UNP200	NDM	NDM	2.934
44	48	49	2:UNP200	NDM	NDM	2.700
45	49	50	2:UNP200	NDM	NDM	1.400
46	50	51	2:UNP200	NDM	NDM	2.800
47	51	52	2:UNP200	NDM	NDM	2.700
48	52	53	2:UNP200	NDM	NDM	2.933
49	53	54	2:UNP200	NDM	NDM	1.467
50	54	55	2:UNP200	NDM	NDM	1.500
51	55	56	2:UNP200	NDM	NDM	3.033
52	56	57	2:UNP200	NDM	NDM	1.467
53	57	58	2:UNP200	NDM	NDM	1.467
54	58	36	2:UNP200	NDM	NDM	2.933
55	1	36	6:H70/70/6	NDM	NDM	2.193
56	17	37	5:H70/70/9	NDM	NDM	2.093



Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

STAVEN

St.	ki	kj	Profiel	Aansl.i	Aansl.j	Lengte
57	37	2	6:H70/70/6	NDM	NDM	2.093
58	2	39	6:H70/70/6	NDM	NDM	2.062
59	39	18	6:H70/70/6	NDM	NDM	2.193
60	18	40	6:H70/70/6	NDM	NDM	2.126
61	40	19	6:H70/70/6	NDM	NDM	2.093
62	19	41	5:H70/70/9	NDM	NDM	2.093
63	41	4	6:H70/70/6	NDM	NDM	2.193
64	41	22	4:H70/70/11	NDM	NDM	2.098
65	22	42	5:H70/70/9	NDM	NDM	2.112
66	42	5	5:H70/70/9	NDM	NDM	2.083
67	5	44	6:H70/70/6	NDM	NDM	2.121
68	44	23	6:H70/70/6	NDM	NDM	2.121
69	23	45	6:H70/70/6	NDM	NDM	2.121
70	45	6	6:H70/70/6	NDM	NDM	2.121
71	6	47	5:H70/70/9	NDM	NDM	2.097
72	47	24	5:H70/70/9	NDM	NDM	2.097
73	24	48	4:H70/70/11	NDM	NDM	2.099
74	48	7	6:H70/70/6	NDM	NDM	2.193
75	48	27	5:H70/70/9	NDM	NDM	2.093
76	27	49	6:H70/70/6	NDM	NDM	2.093
77	8	50	6:H70/70/6	NDM	NDM	2.126
78	50	28	6:H70/70/6	NDM	NDM	2.126
79	28	51	6:H70/70/6	NDM	NDM	2.126
80	51	29	6:H70/70/6	NDM	NDM	2.093
81	29	52	5:H70/70/9	NDM	NDM	2.093
82	52	10	6:H70/70/6	NDM	NDM	2.193
83	52	32	4:H70/70/11	NDM	NDM	2.098
84	32	53	5:H70/70/9	NDM	NDM	2.097
85	53	11	5:H70/70/9	NDM	NDM	2.098
86	11	55	6:H70/70/6	NDM	NDM	2.121
87	55	33	6:H70/70/6	NDM	NDM	2.121
88	33	56	6:H70/70/6	NDM	NDM	2.145
89	56	12	6:H70/70/6	NDM	NDM	2.098
90	12	58	5:H70/70/9	NDM	NDM	2.098
91	58	34	5:H70/70/9	NDM	NDM	2.098
92	34	36	4:H70/70/11	NDM	NDM	2.098
93	36	17	2:UNP200	NDM	NDM	1.600
94	35	36	2:UNP200	NDM	NDM	1.500
95	20	41	2:UNP200	NDM	NDM	1.600
96	41	21	2:UNP200	NDM	NDM	1.500
97	25	48	2:UNP200	NDM	NDM	1.500
98	48	26	2:UNP200	NDM	NDM	1.600
99	30	52	2:UNP200	NDM	NDM	1.600
100	52	31	2:UNP200	NDM	NDM	1.500



Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

STAVEN

St.	ki	kj	Profiel	Aansl.i	Aansl.j	Lengte
101	2	38	3:HEA220	NDM	NDM	1.600
102	38	13	3:HEA220	NDM	NDM	4.400
103	16	51	3:HEA220	NDM	NDM	4.400
104	51	9	3:HEA220	NDM	NDM	1.600
105	3	40	3:HEA220	NDM	NDM	1.600
106	40	14	3:HEA220	NDM	NDM	4.400
107	14	15	3:HEA220	ND	ND	6.000
108	15	49	3:HEA220	NDM	NDM	4.400
109	49	8	3:HEA220	NDM	NDM	1.600
110	12	57	3:HEA220	NDM	NDM	1.500
111	57	13	3:HEA220	NDM	NDM	2.700
112	43	5	3:HEA220	NDM	NDM	1.500
113	14	43	3:HEA220	NDM	NDM	2.700
114	11	54	3:HEA220	NDM	NDM	1.500
115	54	16	3:HEA220	NDM	NDM	2.700
116	46	15	3:HEA220	NDM	NDM	2.700
117	6	46	3:HEA220	NDM	NDM	1.500
118	13	16	3:HEA220	ND	ND	6.000

VASTE STEUNPUNTEN

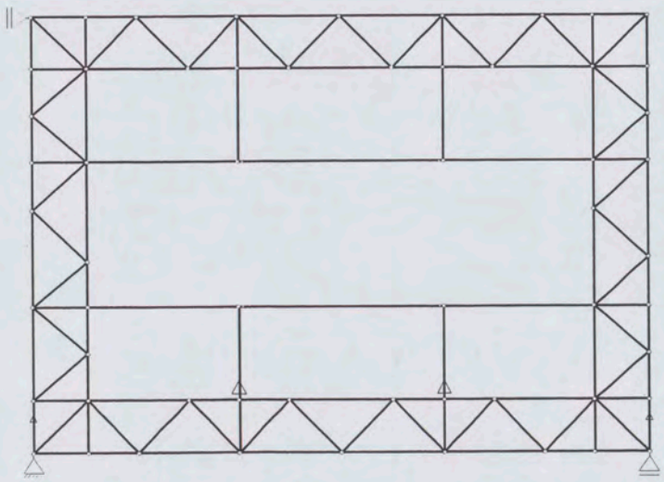
Nr.	knoop	Kode XZR 1=vast 0=vrij
1	1	110
2	4	100
3	10	010

BELASTINGGEVALLEN

B.G.	Omschrijving	Type	e.g.X	e.g.Z
1	windbelasting	1	0.00	0.00

BELASTINGEN

B.G:1 windbelasting



Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

KNOOPBELASTINGEN

B.G:1 windbelasting

Last	Knoop	Richting	waarde
1	12	Z	31.000
2	11	Z	31.000
3	1	Z	16.000
4	10	Z	16.000

GUNSTIGE WERKING PERMANENTE BELASTINGEN

BC	Staven met gunstige werking
1	Geen

BELASTINGCOMBINATIE: 1 wind

1: Uiterste grenstoestand; Fundamentele combinatie

Belastinggeval	Gen. type	factor
1:windbelasting	Permanent	1.50

BELASTINGCOMBINATIE: 2

2: Bruikbaarheidsgrenstoestand; Incidentele combinatie

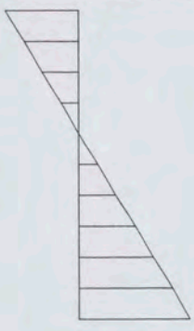
Belastinggeval	Gen. type	factor
1:windbelasting	Permanent	1.00

OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

TUSSENPUNTEN KRACHTEN

Fundamentele combinatie

St.	Kn.	Pos.	Norm.kr.	Dwarskr.	Moment	Moment-plot
1	1		65.82	3.19	-1.91	
1		0.150	65.82	3.19	-1.43	
1		0.300	65.82	3.19	-0.95	
1		0.450	65.82	3.19	-0.48	
1		0.600	65.82	3.19	0.00	
1		0.750	65.82	3.19	0.48	
1		0.900	65.82	3.19	0.96	
1		1.050	65.82	3.19	1.44	
1		1.200	65.82	3.19	1.92	
1		1.350	65.82	3.19	2.40	
1	17		65.82	3.19	2.88	
2	17		44.71	-1.46	2.53	
2		0.270	44.71	-1.46	2.13	
2		0.540	44.71	-1.46	1.74	
2		0.810	44.71	-1.46	1.34	
2		1.080	44.71	-1.46	0.95	
2		1.350	44.71	-1.46	0.55	
2		1.620	44.71	-1.46	0.16	
2		1.890	44.71	-1.46	-0.24	
2		2.160	44.71	-1.46	-0.63	
2		2.430	44.71	-1.46	-1.03	
2	2		44.71	-1.46	-1.42	





Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

TUSSENPUNTEN KRACHTEN

Fundamentele combinatie

St.	Kn.	Pos.	Norm.kr.	Dwarskr.	Moment	Moment-plot
3	2		19.50	0.17	-0.16	
3		0.280	19.50	0.17	-0.11	
3		0.560	19.50	0.17	-0.06	
3		0.840	19.50	0.17	-0.02	
3		1.120	19.50	0.17	0.03	
3		1.400	19.50	0.17	0.08	
3		1.680	19.50	0.17	0.12	
3		1.960	19.50	0.17	0.17	
3		2.240	19.50	0.17	0.22	
3		2.520	19.50	0.17	0.26	
3	18		19.50	0.17	0.31	
4	18		3.37	-0.73	0.34	
4		0.140	3.37	-0.73	0.24	
4		0.280	3.37	-0.73	0.14	
4		0.420	3.37	-0.73	0.03	
4		0.560	3.37	-0.73	-0.07	
4		0.700	3.37	-0.73	-0.17	
4		0.840	3.37	-0.73	-0.27	
4		0.980	3.37	-0.73	-0.37	
4		1.120	3.37	-0.73	-0.48	
4		1.260	3.37	-0.73	-0.58	
4	3		3.37	-0.73	-0.68	
5	3		2.82	0.03	-0.01	
5		0.135	2.82	0.03	-0.00	
5		0.270	2.82	0.03	0.00	
5		0.405	2.82	0.03	0.01	
5		0.540	2.82	0.03	0.01	
5		0.675	2.82	0.03	0.01	
5		0.810	2.82	0.03	0.02	
5		0.945	2.82	0.03	0.02	
5		1.080	2.82	0.03	0.03	
5		1.215	2.82	0.03	0.03	
5	19		2.82	0.03	0.03	
6	19		-0.70	-0.16	0.04	
6		0.135	-0.70	-0.16	0.02	
6		0.270	-0.70	-0.16	-0.01	
6		0.405	-0.70	-0.16	-0.03	
6		0.540	-0.70	-0.16	-0.05	
6		0.675	-0.70	-0.16	-0.07	
6		0.810	-0.70	-0.16	-0.09	
6		0.945	-0.70	-0.16	-0.11	
6		1.080	-0.70	-0.16	-0.13	
6		1.215	-0.70	-0.16	-0.16	
6	20		-0.70	-0.16	-0.18	
7	20		-0.73	0.16	-0.14	
7		0.150	-0.73	0.16	-0.12	
7		0.300	-0.73	0.16	-0.09	
7		0.450	-0.73	0.16	-0.07	
7		0.600	-0.73	0.16	-0.05	

the scale towards document
Image Engineering Scan Reference Chart TE263 Serial No. 546

Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

TUSSENPUNTEN KRACHTEN

Fundamentele combinatie

St.	Kn.	Pos.	Norm.kr.	Dwarskr.	Moment	Moment-plot
7		0.750	-0.73	0.16	-0.02	
7		0.900	-0.73	0.16	-0.00	
7		1.050	-0.73	0.16	0.02	
7		1.200	-0.73	0.16	0.05	
7		1.350	-0.73	0.16	0.07	
7	4		-0.73	0.16	0.09	
8	4		-3.20	-0.14	0.09	
8		0.160	-3.20	-0.14	0.07	
8		0.320	-3.20	-0.14	0.05	
8		0.480	-3.20	-0.14	0.02	
8		0.640	-3.20	-0.14	0.00	
8		0.800	-3.20	-0.14	-0.02	
8		0.960	-3.20	-0.14	-0.04	
8		1.120	-3.20	-0.14	-0.07	
8		1.280	-3.20	-0.14	-0.09	
8		1.440	-3.20	-0.14	-0.11	
8	21		-3.20	-0.14	-0.14	
9	21		-3.32	0.04	-0.07	
9		0.147	-3.32	0.04	-0.07	
9		0.293	-3.32	0.04	-0.06	
9		0.440	-3.32	0.04	-0.06	
9		0.587	-3.32	0.04	-0.05	
9		0.733	-3.32	0.04	-0.04	
9		0.880	-3.32	0.04	-0.04	
9		1.027	-3.32	0.04	-0.03	
9		1.173	-3.32	0.04	-0.03	
9		1.320	-3.32	0.04	-0.02	
9	22		-3.32	0.04	-0.01	
10	22		-2.12	-0.00	-0.02	
10		0.293	-2.12	-0.00	-0.02	
10		0.587	-2.12	-0.00	-0.02	
10		0.880	-2.12	-0.00	-0.02	
10		1.173	-2.12	-0.00	-0.02	
10		1.467	-2.12	-0.00	-0.02	
10		1.760	-2.12	-0.00	-0.02	
10		2.053	-2.12	-0.00	-0.02	
10		2.347	-2.12	-0.00	-0.02	
10		2.640	-2.12	-0.00	-0.02	
10	5		-2.12	-0.00	-0.02	
11	5		-1.15	0.01	-0.02	
11		0.300	-1.15	0.01	-0.02	
11		0.600	-1.15	0.01	-0.02	
11		0.900	-1.15	0.01	-0.02	
11		1.200	-1.15	0.01	-0.02	
11		1.500	-1.15	0.01	-0.01	
11		1.800	-1.15	0.01	-0.01	
11		2.100	-1.15	0.01	-0.01	
11		2.400	-1.15	0.01	-0.01	
11		2.700	-1.15	0.01	-0.00	



Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

TUSSENPUNTEN KRACHTEN

Fundamentele combinatie

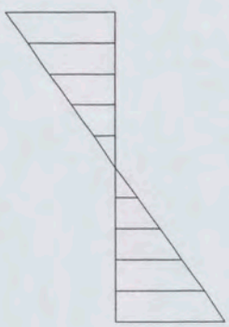
St.	Kn.	Pos.	Norm.kr.	Dwarskr.	Moment	Moment-plot
11	23		-1.15	0.01	-0.00	
12	23		0.63	0.01	-0.01	
12		0.300	0.63	0.01	-0.00	
12		0.600	0.63	0.01	-0.00	
12		0.900	0.63	0.01	0.00	
12		1.200	0.63	0.01	0.00	
12		1.500	0.63	0.01	0.01	
12		1.800	0.63	0.01	0.01	
12		2.100	0.63	0.01	0.01	
12		2.400	0.63	0.01	0.01	
12		2.700	0.63	0.01	0.02	
12	6		0.63	0.01	0.02	
13	6		1.56	-0.01	0.02	
13		0.293	1.56	-0.01	0.02	
13		0.586	1.56	-0.01	0.01	
13		0.880	1.56	-0.01	0.01	
13		1.173	1.56	-0.01	0.01	
13		1.466	1.56	-0.01	0.01	
13		1.759	1.56	-0.01	0.01	
13		2.052	1.56	-0.01	0.00	
13		2.346	1.56	-0.01	0.00	
13		2.639	1.56	-0.01	-0.00	
13	24		1.56	-0.01	-0.00	
14	24		2.59	0.08	-0.00	
14		0.147	2.59	0.08	0.01	
14		0.294	2.59	0.08	0.02	
14		0.440	2.59	0.08	0.03	
14		0.587	2.59	0.08	0.04	
14		0.734	2.59	0.08	0.05	
14		0.881	2.59	0.08	0.07	
14		1.028	2.59	0.08	0.08	
14		1.174	2.59	0.08	0.09	
14		1.321	2.59	0.08	0.10	
14	25		2.59	0.08	0.11	
15	25		2.37	-0.29	0.26	
15		0.160	2.37	-0.29	0.21	
15		0.320	2.37	-0.29	0.16	
15		0.480	2.37	-0.29	0.12	
15		0.640	2.37	-0.29	0.07	
15		0.800	2.37	-0.29	0.03	
15		0.960	2.37	-0.29	-0.02	
15		1.120	2.37	-0.29	-0.07	
15		1.280	2.37	-0.29	-0.11	
15		1.440	2.37	-0.29	-0.16	
15	7		2.37	-0.29	-0.21	
16	7		2.24	0.29	-0.21	
16		0.150	2.24	0.29	-0.16	
16		0.300	2.24	0.29	-0.12	



Project..: SHELL A'dam hal 11C
Onderdeel: stab.krans +7.250

TUSSENPUNTEN KRACHTEN

Fundamentele combinatie

St.	Kn.	Pos.	Norm.kr.	Dwarskr.	Moment	Moment-plot
16		0.450	2.24	0.29	-0.08	
16		0.600	2.24	0.29	-0.03	
16		0.750	2.24	0.29	0.01	
16		0.900	2.24	0.29	0.05	
16		1.050	2.24	0.29	0.10	
16		1.200	2.24	0.29	0.14	
16		1.350	2.24	0.29	0.18	
16	26		2.24	0.29	0.22	
17	26		2.48	-0.04	0.04	
17		0.135	2.48	-0.04	0.03	
17		0.270	2.48	-0.04	0.03	
17		0.405	2.48	-0.04	0.02	
17		0.540	2.48	-0.04	0.02	
17		0.675	2.48	-0.04	0.01	
17		0.810	2.48	-0.04	0.01	
17		0.945	2.48	-0.04	0.00	
17		1.080	2.48	-0.04	-0.00	
17		1.215	2.48	-0.04	-0.01	
17	27		2.48	-0.04	-0.02	
18	27		4.00	0.13	-0.02	
18		0.135	4.00	0.13	-0.01	
18		0.270	4.00	0.13	0.01	
18		0.405	4.00	0.13	0.03	
18		0.540	4.00	0.13	0.05	
18		0.675	4.00	0.13	0.06	
18		0.810	4.00	0.13	0.08	
18		0.945	4.00	0.13	0.10	
18		1.080	4.00	0.13	0.12	
18		1.215	4.00	0.13	0.13	
18	8		4.00	0.13	0.15	
19	8		10.63	0.25	-0.34	
19		0.280	10.63	0.25	-0.28	
19		0.560	10.63	0.25	-0.21	
19		0.840	10.63	0.25	-0.14	
19		1.120	10.63	0.25	-0.07	
19		1.400	10.63	0.25	-0.00	
19		1.680	10.63	0.25	0.07	
19		1.960	10.63	0.25	0.14	
19		2.240	10.63	0.25	0.20	
19		2.520	10.63	0.25	0.27	
19	28		10.63	0.25	0.34	
20	28		21.61	-0.55	0.34	
20		0.140	21.61	-0.55	0.27	
20		0.280	21.61	-0.55	0.19	
20		0.420	21.61	-0.55	0.11	
20		0.560	21.61	-0.55	0.04	
20		0.700	21.61	-0.55	-0.04	
20		0.840	21.61	-0.55	-0.12	
20		0.980	21.61	-0.55	-0.19	

the scale towards document
Image Engineering Scan Reference Chart TE263 Serial No. 546